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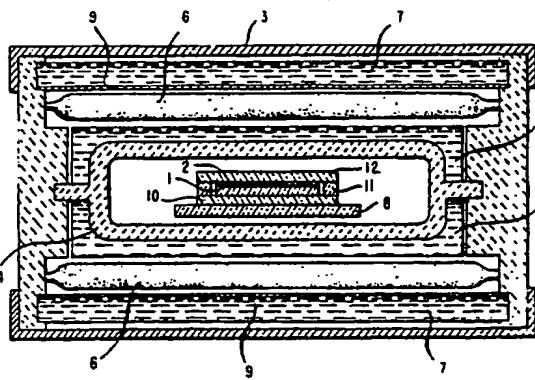
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### ⑯ Procedure and apparatus for annealing of semiconductors.

⑰ This invention is directed to the fabrication of semiconductor devices, especially those comprising III-V and II-VI compound semiconductor materials, and involves annealing, especially Rapid Thermal Annealing (RTA), of semiconductor wafers, especially those implanted with a dopant(s). The invention is also concerned with a black-box implement used in combination with the RTA. The process includes enclosing a wafer (1) to be annealed within a "black-box" comprising components (10,11,12) of a black body material and subjecting the black box with the wafer therein to an RTA. In a preferred embodiment the RTA comprises (a) a pre-anneal step which includes heating to a temperature and for a period sufficient to preheat the wafer so as to reduce thermal shock due to a main annealing step, (b) the main annealing step being at a temperature and for a period sufficient to remove damage caused to said surface by the dopant implantation and to activate implanted dopant, and (c) a post-anneal step carried out at a temperature and for a period sufficient to relieve stresses which may result from the main annealing step. The combined use of the RTA

and the black box leads to wafers substantially free of slip lines and with reproducibly high mobilities and uniform activation.

FIG. 1



## PROCEDURE AND APPARATUS FOR ANNEALING OF SEMICONDUCTORS

Technical Field

The invention is directed to the fabrication of semiconductor devices, especially those comprising III-V and II-VI compound semiconductor materials, which involves annealing of semiconductor wafers.

Background of the Invention

In the production of semiconductor devices, wafers of semiconductor material may be doped with at least one dopant by ion implantation. This process invariably damages the implanted surface. It is desirable to remove this damage so as to present a high quality surface for subsequent processing steps, such as metallization. This is typically achieved by subjecting the implanted wafer to annealing which simultaneously activates the implanted ions.

Conventional long-term furnace annealing leads to a high-quality surface. Unfortunately, the furnace annealing is time and energy consuming, and may result in dopant profile broadening as well as the loss of volatile components (e.g. As from GaAs wafers or P from InP wafers) requiring maintenance of a specific atmosphere over a sample being annealed to compensate for the loss of the volatile component.

Lately, Rapid Thermal Annealing (RTA) is becoming increasingly useful in the processing of implanted semiconductors, especially of semiconductors comprising III-V and II-VI compound semiconductors, including such as GaAs and InP and compound semiconductors lattice-matched to GaAs and InP such as InGaAs, InGaAsP, AlInAs, AlInAsP, etc. In the RTA process, the object being annealed is exposed to heat energy at high temperatures of up to 1100 °C for short periods of time such as from 1 to 30 seconds or more. For example, InP wafers are subjected to temperatures ranging from 700 to 800 °C while GaAs wafers are annealed at temperatures ranging from 800 to 1050 °C.

The RTA method offers the advantage of removing the implantation damage with less dopant profile broadening compared to conventional furnace annealing. However, the RTA process is conducive to slip line formation as well as EN1 traps during the RTA.

Slip lines are regions of a wafer resulting from the introduction of thermoelastic stresses arising from high temperature exposure during the RTA and giving rise to thermoplastic phenomena involving dislocation glide. Since in the RTA method, the

cooling of the sample takes place primarily by radiation, thermal gradients can occur due to variation in radiation intensity from different parts of the sample. For example, the edge of the wafer

5 cools faster than the center due to the comparatively higher radiation from it. As a result, thermal stresses leading to the slip lines can be created by the thermal gradient in the wafer. G. Bentini, L. Correra and C. Donolato in "Defects Introduced in  
10 Silicon Wafers During Rapid Isothermal Annealing: Thermoelastic and Thermoplastic Effects", J. App. Phys. 56 (10), 15 November 1984, pp. 2922-2929, describe formation of slip lines in silicon. This phenomena occurs in III-V and II-VI semiconductor  
15 materials as well. Very often, the slip lines may extend for a considerable distance into the central area of semiconductor wafers, such as 1.3 cm. (0.5 inches) or more from an edge of a wafer about 5 or 7.6 cm. (2.0 or 3.0 inches, respectively) in diameter, resulting in regions which are not suitable for further processing, thus leading to poor device yield.

20 Additionally, EN1 traps may be introduced at higher RTA temperatures. In such compound semiconductors as n-GaAs the EN1 traps are typically introduced by RTA above 800 °C. The EN1 trap is an electron trap with a certain activation energy from the conduction band and results from infrared heating during the RTA. This trap formation is closely related to a rapid heating stage in the RTA process and is never observed after conventional furnace annealing. For more detailed discussion of  
25 EN1 traps, see M. Kazuhara and T. Nozaki, "Study of Electron Traps in n-GaAs Resulting From Infrared Rapid Thermal Annealing", J. Appl. Phys. 59 (9), 1 May 1986, pp. 3131-3136. The formation of electron traps in n-GaAs from RTA has been studied using deep level transient spectroscopy. It has been reported by these authors that in addition to a number of trap levels generally present in as-grown bulk GaAs, a new trap EN1 with an activation energy of 0.20 eV from the conduction band and an electron capture cross section of  $5.4 \times 10^{-16} \text{ cm}^2$ , is formed in encapsulated GaAs annealed at  
30 950 °C in an RTA.

35 It is important that the wafers annealed by RTA should possess not only reproducibly high mobilities and uniform activation, but should also be of morphological quality at least comparable to that obtained with the conventional furnace annealing. Thus, it is desirable to be able to subject the implanted semiconductor wafers to RTA while at the same time obtaining a high quality surface without any slip lines. Additionally, it is desirable to substantially avoid presence of EN1 trapped de-

fects in the RTA treated wafers.

The problems outlined above may be overcome by means of the invention set out in the claims.

In an exemplary process according to the invention, a wafer to be annealed is placed within a "black-box" comprising a base, a guard ring and a lid which is then positioned within an annealing chamber. The black-box is of a material which substantially absorbs incident radiation energy and dissipates energy principally by radiation. The RTA of the wafer annealed within the black-box results in wafers substantially free of slip lines. RTA carried out as a three-step anneal leads to reproducibly high mobilities and uniform activation. The three-step RTA includes a pre-anneal step at a temperature and for a period of time sufficient to reduce thermal shock to the wafer which otherwise may result from higher annealing temperatures, a main anneal step at a temperature and for a period sufficient to remove damage caused to the semiconductor surface by ion implantation and to activate dopant ions, and a post-anneal step at a temperature and for a period sufficient to relieve stresses resulting from the main-anneal step. The use of the three step RTA in combination with the black-box leads to wafer substantially free of slip lines and with reproducibly high mobilities and uniform activation.

#### Brief Description of the Drawings

FIG. 1 is a partial perspective view of a heating chamber of a representative annealing apparatus, including some of its components used in conducting the RTA in accordance with the invention.

FIG. 2 is an exploded view of components of a "black-box" annealing implement being used for annealing semiconductor wafers in accordance with the invention.

FIG. 3 is a graph of a three-step annealing cycle for annealing Si-implanted GaAs wafers.

FIGs. 4, 5, 6 and 7 compare four different variants of effects of RTA on the morphological quality of RTA treated GaAs wafers.

FIG. 8 discloses a carrier concentration profile vs depth profile for exemplary GaAs implanted with a dose of  $3 \times 10^{12} \text{ cm}^{-2}$  of  $^{29}\text{Si}$  at 60 KeV and annealed using a three-step cycle of 650°C for 30s - 950°C for 10s - 850°C for 30s.

#### Detailed Description

This invention is concerned with the fabrication of semiconductor devices comprising III-V and II-VI compound semiconductor materials which involves

Rapid Thermal Anneal (RTA) of semiconductor wafers implanted with a suitable dopant. A technique and apparatus for annealing wafers by RTA with avoidance of slip lines and with reproducibly high mobilities and uniform activation are described below. Si-implanted GaAs wafers are being used as exemplary semiconductor wafers for illustrating the invention. Other semiconductor materials and other dopants may be treated with logical modifications utilising the hereinbelow described teachings.

Wafers used in this illustration were originally undoped, (100) oriented, chem-mechanically polished, semi-insulating GaAs wafers that were about 5 cm (2 inches) in diameter and about 500  $\mu\text{m}$  (20 mils) thick. Approximately 5  $\mu\text{m}$  of the surface thickness of each wafer was removed by etching in a freshly prepared solution of 5  $\text{H}_2\text{SO}_4$  :  $\text{H}_2\text{O}_2$  :  $\text{H}_2\text{O}$  prior to ion implantation.  $^{29}\text{Si}$  was implanted at room temperature in a nonchanneling direction. The dose and energy of the implants were  $3 \times 10^{12} \text{ cm}^{-2}$  and 60 KeV, respectively. Other doses ranging from  $3 \times 10^{12}$  to  $5 \times 10^{15} \text{ cm}^{-2}$  and energies ranging from 30 to 800 KeV may be used to implant these ions at room temperature. Prior to the RTA, the implanted wafers were capped (encapsulated) with a film of e-beam deposited glass in a thickness within a range from 10 to 500 nm. Phosphosilicate glass (PSG) containing from 1 to 15 mole percent  $\text{P}_2\text{O}_5$ , preferably 2 to 10 mole percent  $\text{P}_2\text{O}_5$ , is most suitable for use in RTA because of its excellent protective characteristics. For annealing purposes, a PSG film within a range of from 30 to 150 nm, typically approximately 100 nm thick, is adequate.

Presence of  $\text{P}_2\text{O}_5$  in  $\text{SiO}_2$  glass lowers its softening temperature and increases its thermal expansion coefficient, thus reducing stress during thermal annealing, especially by RTA. Also, presence of phosphorus inhibits further diffusion of, e.g. ion implanted dopants on annealing. The  $\text{P}_2\text{O}_5$  content of a PSG used as a barrier layer in the annealing procedure is selected such that the softening temperature is below an anneal temperature, but the melting point of an equivalent crystalline material is above the anneal temperature. Under these conditions, the glass layer forms a good barrier without stressing the semiconductor surface.  $\text{P}_2\text{O}_5$  content above 15 mole percent still causes lowering of the stress, but the film might not be chemically inert. Amounts below 1 mole percent may still significantly reduce stress, however, only marginally reducing the glass softening temperature. Since for many applications, annealing is desired below 1200°C (e.g. 800 to 1050°C for GaAs), a typical useful range for the amount of  $\text{P}_2\text{O}_5$  in PSG ranges from 2 to 10 mole percent. A more detailed discussion for the selection of the amount of  $\text{P}_2\text{O}_5$  in PSG may be found in U. S.

Patent 4,731,293 issued on March 15, 1988 to D. T. Ekholm et al.

The phosphosilicate glass may be very effectively and inexpensively prepared for use in e-beam deposition by sol-gel technique disclosed in a co-pending U.S. patent application Serial No. 345,924 filed May 1, 1989 in the name of D. A. Fleming et al. (Case 1-17-42-125-22). Some other glasses, such as borosilicate or commercially obtainable Vycor® (3%  $B_2O_3$ , 1%  $Al_2O_3$  and 96%  $SiO_2$ , all by weight) may also be used for encapsulation. The use of borosilicate glass in fabrication of such devices as avalanche photodiodes is disclosed in U.S. Patent No. 4,819,039 issued April 4, 1989 in the name of G. Chi et al. The use of PSG glass in preparation of various semiconductor devices including avalanche photodiodes is disclosed in the above-mentioned U. S. Patent 4,731,293.

Wafers, 1, having an encapsulating film, 2, over an implanted surface, were annealed in an annealing apparatus under flowing dry inert gas, such as nitrogen ( $N_2$ ), argon, forming gas, etc. Apparatus used for the RTA should be capable of providing thermal energy sufficient to preheat a semiconductor sample to a temperature intermediate a starting, e.g. room, temperature and a peak annealing temperature, and of providing high thermal energy, e.g. up to 1100-1200 °C suitable for said peak annealing for a period ranging from 1 to 30 seconds. A microprocessor controlled HEATPULSE™ 410 halogen lamp annealing system, commercially available from AG Processing Technologies, Inc., 1325 Borregas Avenue, Sunnyvale, California, 94089, U.S.A. is suitable for this purpose.

A representative annealing apparatus includes a heating chamber, 3, shown in FIG. 1. The heating chamber includes a quartz isolation tube, 4, a lower and an upper bank of high-intensity tungsten-halogen lamps, 6, and conduits, 7, for carrying a suitable cooling fluid, such as water. Lamps 6 emit pulsed radiant energy to heat wafer 1 placed on a tray or susceptor, 8, within the isolation tube. At low temperatures the wafer absorbs visible light, and at high temperatures it absorbs infrared radiation. Reflective surfaces, 9, are provided to reflect the heat energy toward the isolation tube and enhance the uniformity of heat energy distribution.

Thermal processing occurs in isolation tube 4 between upper and lower banks of lamps 6. Tray 8 of suitable material, such as quartz, is removably positioned within isolation tube 4, and is used for supporting implanted and encapsulated wafer 1, being processed, within the tube. To monitor the annealing, the apparatus may be equipped with a pyrometer (not shown) and a thermocouple (not shown). The annealing temperature is typically controlled with pyrometer sensing, while wafer temperatures up to within a range of 625-675 °C are

monitored with a thermocouple, such as a chromel-alumel thermocouple. The thermocouple may be mounted in a suitable manner, such as on tray 8 beside the wafer, in contact with an underside of the wafer, or embedded in the wafer.

In accordance with the invention, implanted and encapsulated wafer 1 prior to being placed on tray 8 is enclosed within an implement which may be entitled a "black-box". The implement comprises three components: a base or plate, 10, for supporting wafer 1, a guard ring, 11, for encompassing the wafer, and a lid or cover, 12, for sealing a cavity formed by the base and the guard ring. The black box components are of a "black-body" material which absorbs substantially all incident radiation energy (i.e. the emission of lamps 6) and dissipates the absorbed energy principally by radiation. The black box components should also be of a material which is stable under operating conditions and inert with respect to the gaseous environment, e.g.  $N_2$ . In the illustrative example, the black box components are made of a material selected from graphite or silicon. Whenever it is desired to reduce the possibility of contamination of the material of the wafer by the material(s) of the black box components, especially at higher RTA temperatures, at least the internally facing surfaces of these components may be covered by an encapsulating glass film. The coating may be applied in a suitable thickness, such as 100-500 nm thick. The coating may be preferably of the same glass material as is used for capping the wafer. However, other encapsulating materials such as Vycor® or  $SiO_2$  may be used as well.

The inside diameter dimension of guard ring 11 is somewhat larger than the dimension of wafer 1 to be annealed so as to allow for a small clearance between the implanted wafer and the guard ring. The clearance is provided to allow for the expansion of the wafer within the cavity while allowing efficient, evenly distributed transfer of heat between the guard ring of the black box and the wafer. For similar reasons, the height of the guard ring is somewhat greater than the thickness of the implanted wafer so that lid 12 is also spaced from implanted wafer 1. Typically for a wafer about 500  $\mu m$  thick, the guard ring is from 600 to 900  $\mu m$  high. This provides at least 100  $\mu m$  clearance between the wafer and the lid. A similar clearance is provided between the inner walls of the guard ring and the wafer. The outside dimension of the guard ring, and thus, of the base and the lid, may be selected so as to fit within the boundaries of retainers 13 positionable on the tray within selected spacing apertures 14 (FIG. 2). Typically each of the base, lid and walls of the guard ring is from 600 to 1000  $\mu m$  thick. Thus, for an implanted wafer approximately 5 cm. (2 inch) in diameter, the inside

dimension of the guard ring is approximately 5.7 cm. (2.25 inches) in diameter and the outside dimension of the base, the guard ring and the lid is approximately 7.6 cm. (3 inches) in diameter. For an implanted wafer approximately 7.6 cm. (3 inches) in diameter, the inside dimension of the guard ring is approximately 8.3 cm. (3.25 inches) in diameter and the outside dimensions of the black-box components are approximately 10 cm. (4 inches) in diameter each. Different respective outside dimensions may be selected as well so as to fit a fastening arrangement of the tray being used.

Prior to annealing, base 10, is placed on tray 8, guard ring 11 is placed on base 10, the implanted and encapsulated wafer 1 with the implanted side facing up is placed on base 10 within a cavity formed by guard ring 11, and then lid 12 is placed over guard ring 11 to enclose wafer 1 within the so-formed black-box. Alternatively, wafer 1 may be placed on base 10 prior to placing the guard ring on the base or the black box with wafer 1 may be assembled prior to placing the black box on the tray.

After establishing a flow of dry inert gas, such as N<sub>2</sub>, through isolation tube 4 and, thus, over the black box, wafer 1 was subjected to an RTA. In the particular example, the annealing cycle was a three-step anneal cycle consisting of a pre-anneal step, main annealing pulsed step and a post-anneal step, followed by a cool-down as is shown in FIG. 3.

The pre-anneal step is conducted by raising the temperature to within a range of from 625 to 675 °C and maintaining this temperature for a period sufficient to preheat not only the box, but also the wafer within the box. This reduces the effects of the thermal shock to which the wafer would be exposed upon being subjected directly to the higher annealing temperature. Preferably, the pre-anneal step is conducted at about 650 °C for a period of about 30 seconds. The main annealing pulsed step is conducted at temperatures ranging from 900 to 1000 °C for a period sufficient to anneal out the damage in the surface of wafer 1 caused by the ion implantation. A period of time of up to 50 seconds could be useful, with a period falling within a range of from 5 to 20 seconds being most suitable. Preferably, the main annealing pulse step is conducted at 950 °C peak temperatures for about 10 seconds. The post-anneal step is conducted at a temperature within a range of from 825 to 875 °C, for a period of time sufficient to relieve stresses which may be caused by the high temperature anneal. Preferably, the post-anneal is conducted by maintaining the pulse-annealed wafer at about 850 °C for a period of about 30 seconds. After the post-anneal step, the wafer is permitted to cool down to at least 550 °C at a rate of from 5 to

50 °C/second. Typically the cool-down proceeds at a cooling rate of approximately about 30 °C/second or less. Annealed wafers 1 are removed from heating chamber 3 when their temperature falls below 200 °C. After annealing, encapsulant 2 on annealed wafer 1 may be retained or, if an unencapsulated surface is desired for subsequent device processing, the encapsulant may be removed using HF:H<sub>2</sub>O etching solution.

10 To determine the effectiveness of the main annealing temperature and time on slip lines, a number of wafers were annealed at peak temperatures ranging from 925 to 1000 °C for times varying between 5 and 20 seconds. All wafers annealed in this way, when examined with an optical microscope, were entirely free from thermal damage. In order to examine the wafers for slip lines, they were etched in molten (300 °C) KOH for 20 min.

15 The effectiveness of the use of the black box with a guard ring and lid of graphite or silicon in eliminating slip lines is shown in FIGS. 4, 5, 6 and 7. In this experiment, four implanted and encapsulated wafers (shown in FIGS. 5, 6 and 7, respectively) from the same GaAs boule were annealed using the three-step cycle including pre-anneal step at 650 °C for about 30 seconds, main annealing pulse step with peak temperature of 950 °C for about 10 seconds and post-anneal step at 850 °C for about 30 seconds. Wafers shown in FIGS. 4, 6 and 7, respectively, were permitted to cool from the post-anneal temperature of 850 °C at a natural cooling rate of about 30 °C/second, while wafer shown in FIG. 5 was permitted to cool at a cooling rate of about 10 °C/second.

20 30 35 40 45 50 55 Wafer shown in FIG. 4 was annealed inside a black box cavity formed by a base of silicon and a guard ring and a lid of graphite. The topographic distribution of the damage due to slip lines in this wafer was limited to only a small boundary region comprising of less than 10% of the surface. Wafer B was annealed using the same type of the black box, but was permitted to cool down from 850 °C to about 600 °C at a slower rate of cooling (=10 °C/sec) than the first wafer. The results indicate that under these conditions, the wafer was totally free of slip lines. The reproducibility of this process was established with more than 20 wafers which were annealed at peak temperatures ranging between 925 and 1000 °C. The mere use of slow cooling rate without the graphite guard ring and lid was unsuccessful in eliminating slip lines. Results obtained with a guard ring and lid of silicon were also highly satisfactory, comparable to those obtained with the guard ring and lid of graphite.

For comparison purposes wafer C was annealed upon a silicon base, but without any guard ring or lid. The slip line density in this wafer was so high as to essentially render it useless for device

fabrication. Wafer D was annealed inside a cavity of a box formed by a fused  $\text{SiO}_2$  guard ring and a silicon lid. In this case, although there was a slight reduction in the density of slip lines (relative to the density without the guard ring and lid), more than 75% of the wafer was not fit for device use. Results obtained with a guard ring of alumina and a silicon or graphite lid were also unsatisfactory, comparable to those obtained with the guard ring of fused silica.

These examples show that the use of a black-box implement including a guard ring and a lid of a black body material, such as either graphite or silicon, effectively eliminates the slip damage. A guard ring made of fused silica or alumina were found to be ineffective in preventing the slip lines. Similarly, unfavorable results were obtained when using guard ring and lid made of fused silica or alumina.

The advantage of the three step anneal over a two step anneal including a pre-anneal and a main annealing step was explored in the following way. A number of 5 cm. (2 inch) diameter wafers were split into two halves. One piece from each wafer was activated using a two step anneal of pre-anneal at  $650^\circ\text{C}$  for about 30s followed by the main annealing at  $950^\circ\text{C}$  for about 10s. The other piece of the same wafer was annealed using the three step cycle depicted in FIG. 3. Both anneal sets were carried out with the black box with base of silicon and with guard ring and lid of graphite. When examined for slip lines, both pieces were found to be slip-free. This shows that the black box is effective in avoiding slip lines with either two-step or three-step RTA.

However, the mobility and activity characteristics, obtainable from the two-step anneal were not as effective as those obtainable from the three-step anneal. Activation resulting from either two-step or three-step anneal was comparable and nearly 100%. However, average mobilities obtainable with two-step anneal were much lower than with the three-step anneal.

Carrier concentration versus depth profiles were obtained from C-V measurements on a mercury probe which was calibrated against a bulk n-GaAs standard using Ti-Au Schottky-barrier diodes. Results of C-V measurements yielded carrier concentration versus depth profiles which were in excellent agreement with theoretical LSS profile curves for both halves indicating nearly 100%-activation. A typical depth profile obtained from three-step annealing of 7.6 cm. (3 inch) diameter GaAs wafer is shown in FIG. 5 indicating the nearly 100%-activation. The LSS profile is given by the solid line. The solid curve represents the theoretical or LSS curve and is obtained by using the projected range and projected standard deviation

derived from the Lindhard, Scharff and Schlott theory. Projected Range Statistics, Semiconductors and Related Materials, 2nd Edition, by James F. Gibbon, William S. Johnson and Steven W. Mylroie; Halstead Press, John Wiley and Sons, Inc., New York.

Hall effect and sheet resistivity measurements were performed using the Van der Pauw method to examine the sheet carrier concentration ( $N_g$ ) and average sheet mobility ( $\mu_m$ ) of the implanted active layer. Hall measurements on the two-step annealed pieces gave average mobilities ranging from  $1500\text{-}2000 \text{ cm}^2/\text{V.S.}$ , whereas the three-step annealed samples had mobilities between  $2500\text{-}3000 \text{ cm}^2/\text{V.S.}$  This difference may be explained as follows. Local variation of mobility on a given wafer of GaAs is commonly observed and related to the variation of dislocations across the sample. There is a possibility of formation of trapped lattice defects during the anneal in view of the fact that rapid heating and cooling steps are involved in the RTA process. The presence of such trapped defects would result in poor mobility of majority carriers in the implanted layer. Thus, low measured mobilities on nearly 100%-activated layers obtained with the two-step anneal cycle (pre-anneal step at  $650^\circ\text{C}$  for about 30 seconds, followed by main annealing pulsed step at  $950^\circ\text{C}$  for about 10 seconds) may be attributed to the presence of EN1 traps.

Activated layers with reproducibly high mobility were obtained by the use of a three step anneal cycle in which the final step consisted of  $850^\circ\text{C}$  anneal for about 30 seconds. Since higher mobilities are observed in wafers activated using a three-step anneal cycle, it is not unreasonable to assume that the EN1 traps did not form in this process. Otherwise, the presence of EN1 traps would result in lower mobility due to scattering of carriers. Nevertheless, it could be also assumed that if any EN1 trapped defects did result from the main annealing pulsed step, they must have been removed by the post anneal step. Indeed, this is supported by the observation by M. Kuzuhara and T. Nozaki, mentioned before, that the EN1 trap was annihilated by long term (duration  $> 25\text{s}$ ) annealing.

## Claims

1. Apparatus for use in a semiconductor annealing process CHARACTERISED BY components of black-body material stable under annealing conditions, said components including a base (10), an annular guard ring (11) and a lid (12) such that when the guard ring is positioned on the base and the lid is positioned on the guard ring, the components form a container (hereinafter referred to as a "black-box") containing a cavity for fully enclosing

a semiconductor wafer (1) to be annealed.

2. Apparatus as claimed in claim 1 in which said black-body material comprises graphite or silicon.

3. Apparatus as claimed in claim 1 or claim 2 in which surfaces of the said components which constitute the internal surfaces of the black-box are encapsulated with a layer of encapsulating material.

4. Apparatus as claimed in claim 3 in which said encapsulating material is selected from the group consisting of phosphosilicate glass, borosilicate glass,  $\text{SiO}_2$ , and a glass consisting of 3%  $\text{B}_2\text{O}_3$ , 1%  $\text{Al}_2\text{O}_3$  and 96%  $\text{SiO}_2$  by weight.

5. Apparatus as claimed in claim 4 in which the encapsulating material comprises phosphosilicate glass comprising 2-10 mole percent  $\text{P}_2\text{O}_5$ .

6. A semiconductor fabrication process comprising subjecting a semiconductor wafer to an annealing procedure CHARACTERISED IN THAT the annealing procedure is carried out with the wafer enclosed in the cavity of a black-box constituted by apparatus as claimed in any of the preceding claims.

7. A process as claimed in claim 6 wherein the annealing procedure is a rapid thermal anneal (RTA).

8. A process as claimed in claim 7 in which said RTA includes in sequence, a pre-anneal step, a main annealing step, and a post-anneal step, the pre-anneal step being conducted at a temperature and for a period sufficient to reduce any thermal shock to the semiconductor material which may result from the main-annealing step, and the post-anneal step being conducted at a temperature and for a period sufficient to relieve stresses which may result from the main-annealing step.

9. A process as claimed in claim 8 in which said compound semiconductor material comprises GaAs, said RTA includes exposure of the black-box with the wafer therein in succession to the pre-anneal step in the temperature range 625 to 675°C for a period in the range 20 to 40 seconds, the main annealing step at a peak temperature within the range 900 to 1000°C for a period in the range 5 to 20 seconds, and the post-anneal step in the temperature range 825 to 875°C for a period in the range 25 to 35 seconds, followed by cool down at a rate in the range 5 to 50°C per second.

10. A process as claimed in claim 9 in which said cool-down is at a rate not exceeding 30°C per second.

11. A process as claimed in claim 10 in which said cool-down is at a rate of about 10°C per second.

12. A process as claimed in any of claims 6 to 11 wherein the wafer has dopant ions implanted into at least one selected area of at least one surface thereof and a layer of encapsulating ma-

terial (2) over said surface, said annealing procedure being conducted at a temperature and for a period sufficient to remove damage caused to the said surface by the implantation and to activate said dopant ions.

13. A process as claimed in claim 12 in which said encapsulating material on said wafer surface comprises a glass selected from phosphosilicate glass, borosilicate glass and a glass consisting of 3%  $\text{B}_2\text{O}_3$ , 1%  $\text{Al}_2\text{O}_3$  and 96%  $\text{SiO}_2$  by weight.

14. A process as claimed in claim 13 in which said encapsulating material on said wafer surface comprises phosphosilicate glass comprising 2-10 mole percent  $\text{P}_2\text{O}_5$ .

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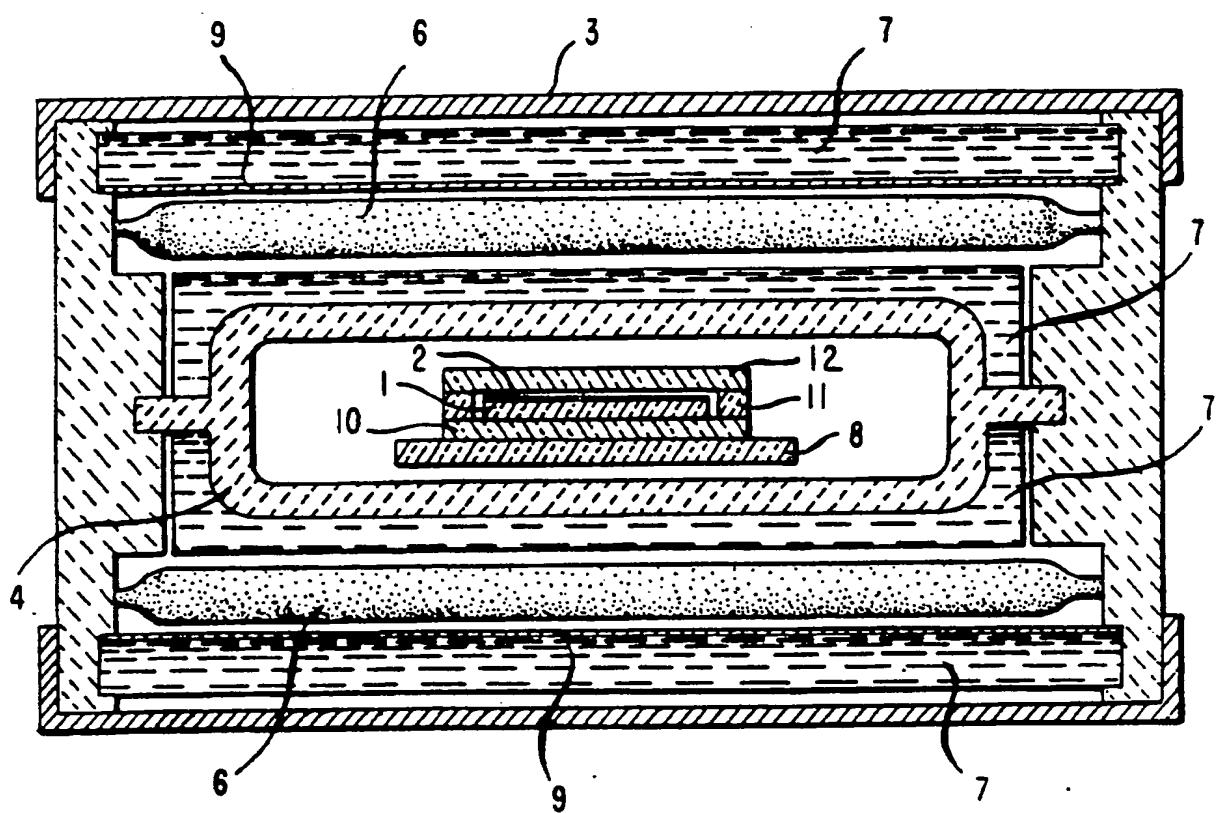
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FIG. 1



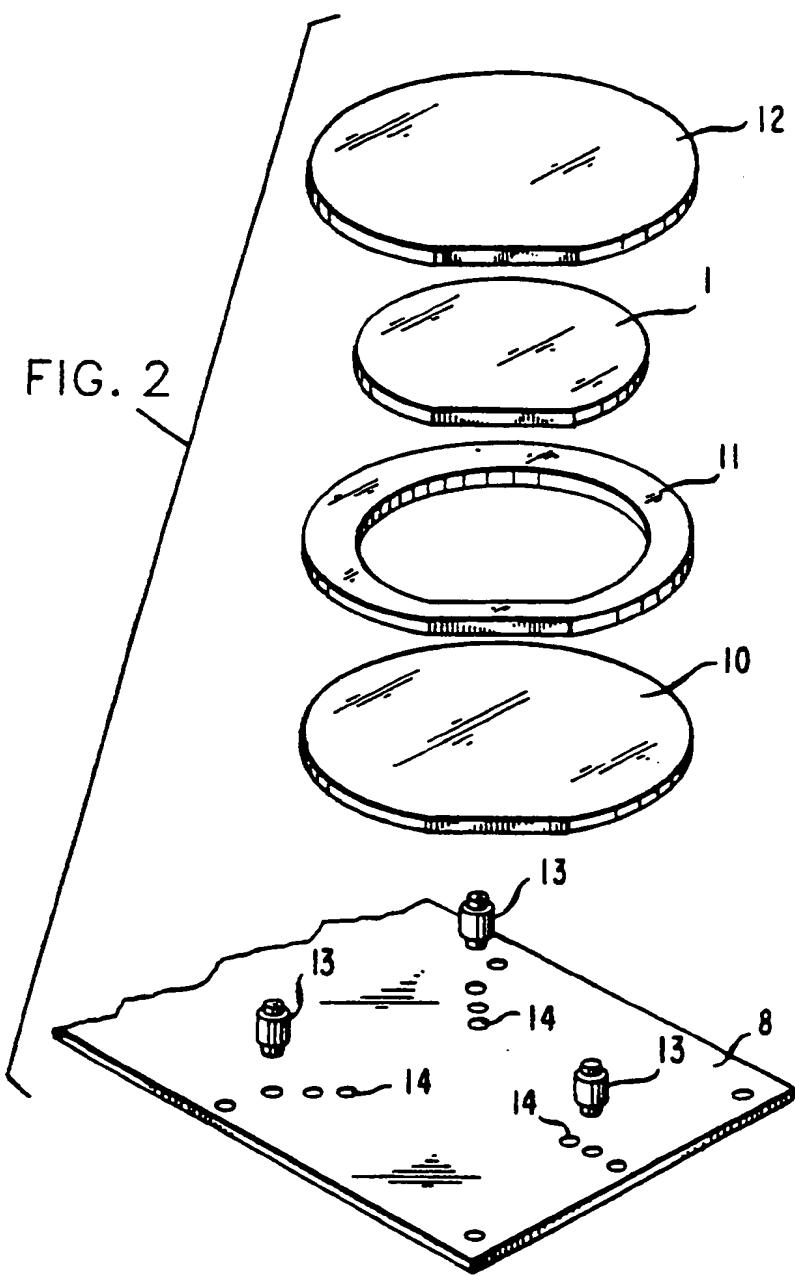


FIG. 3

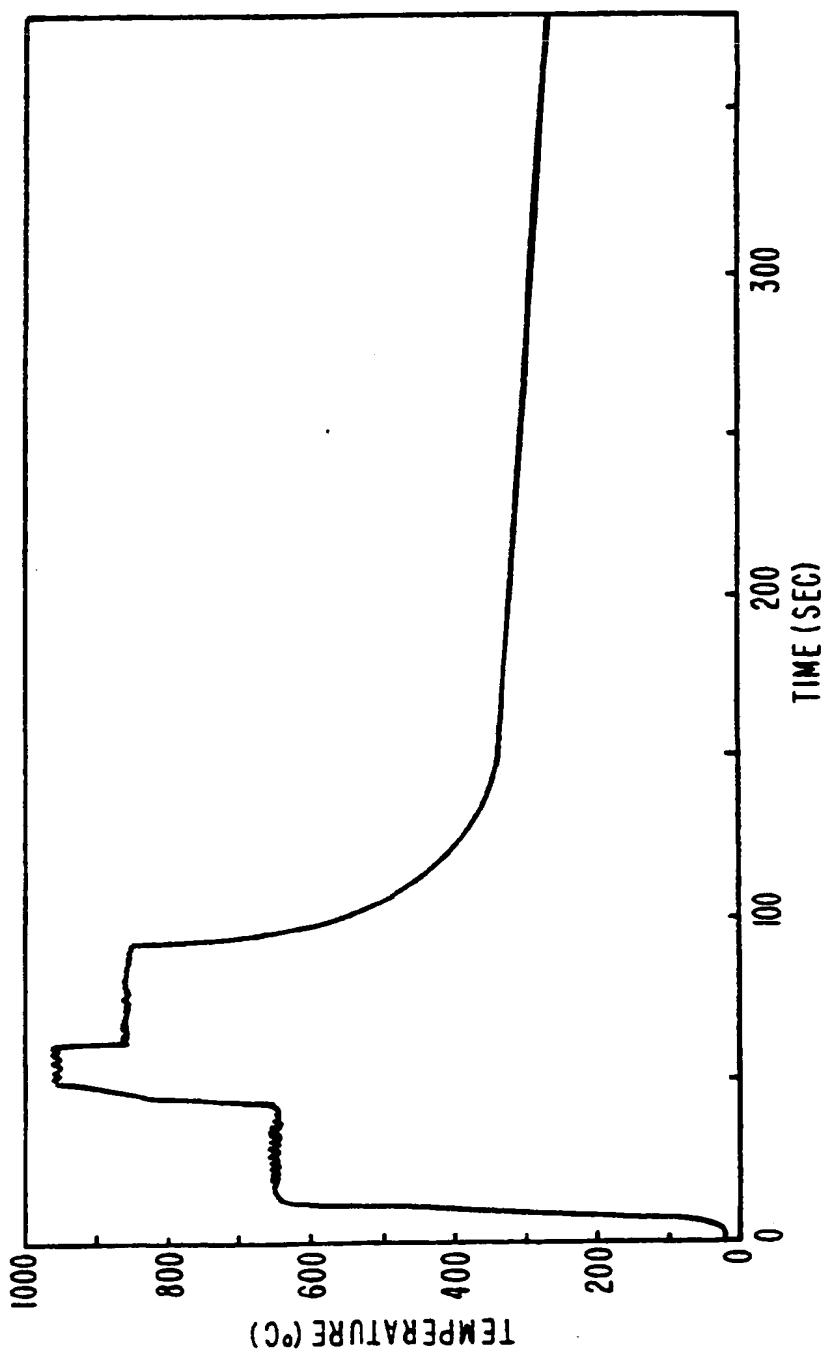
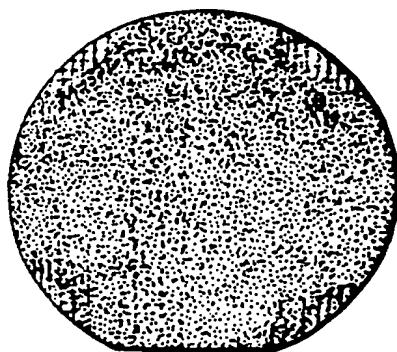
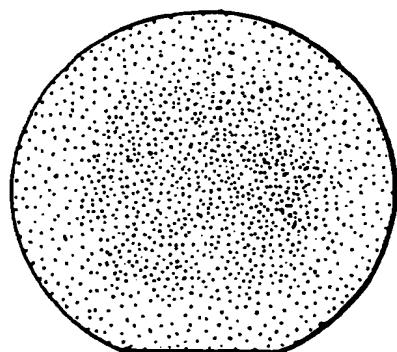


FIG. 4



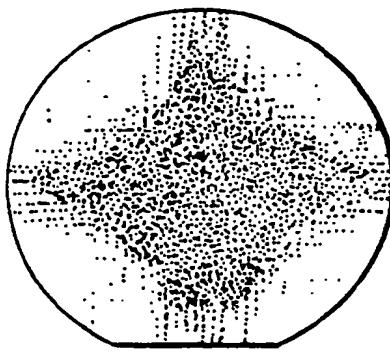
GRAPHITE RING AND LID

FIG. 5



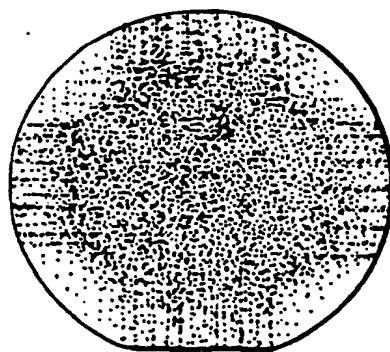
GRAPHITE RING AND LID  
SLOW COOLING

FIG. 6



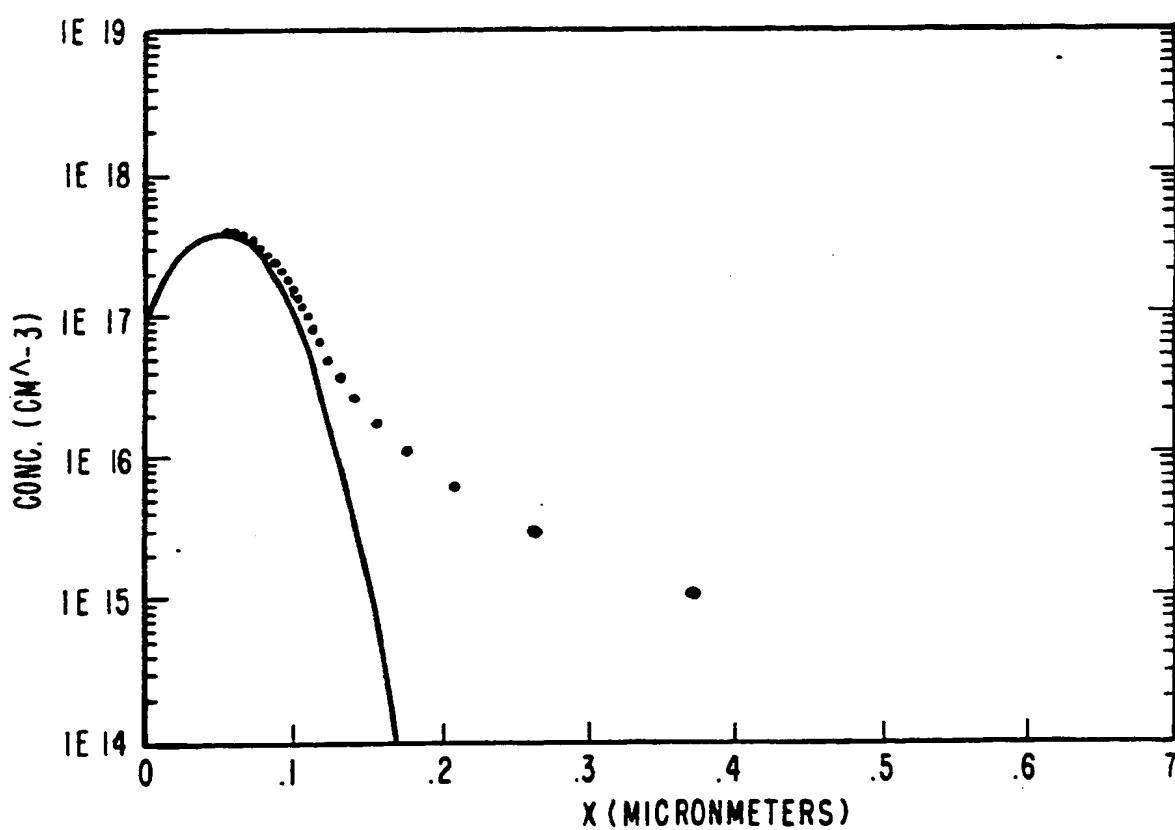
NO RING

FIG. 7



QUARTZ RING

FIG. 8



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⑪ Publication number:

0 399 662 A3

⑫

## EUROPEAN PATENT APPLICATION

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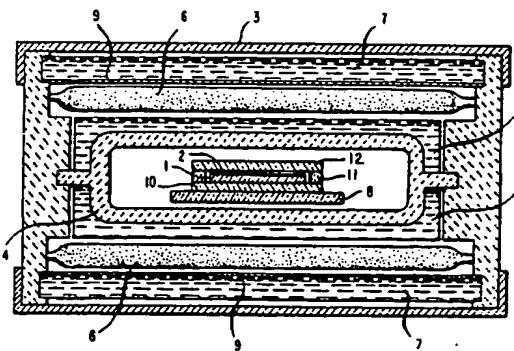
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㉕ Procedure and apparatus for annealing of semiconductors.

㉖ This invention is directed to the fabrication of semiconductor devices, especially those comprising III-V and II-VI compound semiconductor materials, and involves annealing, especially Rapid Thermal Annealing (RTA), of semiconductor wafers, especially those implanted with a dopant(s). The invention is also concerned with a black-box implement used in combination with the RTA. The process includes enclosing a wafer (1) to be annealed within a "black-box" comprising components (10,11,12) of a black body material and subjecting the black box with the wafer therein to an RTA. In a preferred embodiment the RTA comprises (a) a pre-anneal step which includes heating to a temperature and for a period sufficient to preheat the wafer so as to reduce thermal shock due to a main annealing step, (b) the main annealing step being at a temperature and for a period sufficient to remove damage caused to said surface by the dopant implantation and to activate implanted dopant, and (c) a post-anneal step carried out at a temperature and for a period suffi-

cient to relieve stresses which may result from the main annealing step. The combined use of the RTA and the black box leads to wafers substantially free of slip lines and with reproducibly high mobilities and uniform activation.

FIG. 1





European Patent  
Office

EUROPEAN SEARCH REPORT

Application Number

EP 90 30 4436

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl.5)						
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim							
A	US-A-4 725 565 (OREN ET AL.) * column 2, line 48 - column 3, line 9; figure 1 * ----	1,2,6	H01L21/00 H01L21/324						
A	APPLIED PHYSICS LETTERS. vol. 48, no. 23, 9 June 1986, NEW YORK US pages 1623 - 1625; C.A. ARMIENTO AND F.C. PRINCE: 'Capless rapid thermal annealing of GaAs using an enhanced overpressure proximity technique' * the whole document *	1,2,6							
A	APPLIED PHYSICS LETTERS. vol. 47, no. 3, 1 August 1985, NEW YORK US pages 304 - 306; R.T. BLUNT, M.S.M. LAMB AND R. SZWEDA; 'Crystallographic slip in GaAs wafers annealed using incoherent radiation' * the whole document *	1,2,6							
	-----		TECHNICAL FIELDS SEARCHED (Int. Cl.5)						
			H01L						
<p>The present search report has been drawn up for all claims</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 33%;">Place of search</td> <td style="width: 33%;">Date of completion of the search</td> <td style="width: 34%;">Examiner</td> </tr> <tr> <td>THE HAGUE</td> <td>09 JANUARY 1992</td> <td>BOLDER G.J.A.</td> </tr> </table>				Place of search	Date of completion of the search	Examiner	THE HAGUE	09 JANUARY 1992	BOLDER G.J.A.
Place of search	Date of completion of the search	Examiner							
THE HAGUE	09 JANUARY 1992	BOLDER G.J.A.							
<b>CATEGORY OF CITED DOCUMENTS</b> X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons ▲ : member of the same patent family, corresponding document							